

Novel high-gradient accelerating structures

- **Monday**
Introduction to accelerating structures
Traditional [iris-loaded] accelerating structures
Accelerating structure parameters
Introduction to simulations
Computer Lab: Basic examples of simulations (MW simulations)
- **Tuesday**
Dielectric loaded accelerating (DLA) structures
Wakefield Acceleration
Discussion of DLA simulations (MW)
Computer Lab: Basic examples of simulations
- **Wednesday**
Power Extraction. Two beam acceleration
Particle studio examples
Computer Lab: Simulation of DLA. Optimization
Computer Lab: Introduction to Photonic Crystals (simulations)
- **Thursday**
Photonic Crystals General Theory
Photonic Band Gap (PBG) accelerating structures
Computer Lab: MW Simulations of PBG
Computer Lab: Final project (simulation / optimization of accelerating structure)
- **Friday**
Special topics: Beam Break UP. High order mode suppression
Exotic structures. Metamaterials for accelerator applications
Conclusions and final project results

Specifics for this course

- No beam dynamics (until Friday). *Almost* all the time we treat the beam as one macro particle
- High gradient structures
- Emphasis on simulations
- We can adjust the material based on *your* feedback
-

Introduction to accelerating structures

Sergey Antipov and Chunguang Jing

outline

- Brief Introduction
- Electrodynamics
 - Maxwell's equations. Waveguides. Eigenmodes.
 - Dispersion curves. S-parameters. Fourier transforms.
 - Particle interaction. Cherenkov radiation.
- Standard accelerating structures
 - The Floquet theorem. Iris – loaded waveguide
 - Accelerating parameters

Accelerators

Table 1.1. Worldwide inventory of accelerators, in total 15,000.

Category	Number
Ion implanters and surface modifications	7000
Accelerators in industry	1500
Accelerators in non-nuclear research	1000
Radiotherapy	5000
Medical isotopes production	200
Hadron therapy	20
Synchrotron radiation sources	70
Nuclear and particle physics research	110

*U. Amaldi Europhysics News, June 31, 2000

Examples of Accelerator application

- Ion implantation for semiconductors
- Harden cutting tools / reduction of friction in metal parts, bio-materials and implants
- Deep welding for dissimilar metals
- Precision cutting and drilling
- Medical product sterilization
- Food and waste irradiation
- Cross – linking and polymerization
- Waste water remediation
- Cargo examination
- Oil well logging
- Radioisotope production (calibration, medical)
- Synchrotron radiation
- Gemstone color enhancement (topaz, diamonds)

>99% of
accelerators
are in industry

*Robert Hamm, 2010
at High Energy Physics
Advisory Panel

Maxwell's equations

$$\left\{ \begin{array}{l} \nabla \cdot \vec{B} = 0 \\ \nabla \cdot \vec{D} = 4\pi\rho \\ \nabla \times \vec{E} = -\frac{1}{c} \frac{\partial \vec{B}}{\partial t} \\ \nabla \times \vec{H} = \frac{4\pi}{c} \vec{j} + \frac{1}{c} \frac{\partial \vec{D}}{\partial t} \end{array} \right. \quad \text{Assume:} \quad \vec{B} = \mu \vec{H} \quad \vec{D} = \epsilon \vec{E}$$

$$\begin{aligned} \nabla \times \nabla \times \vec{E} &= -\frac{\mu}{c} \frac{\partial \nabla \times \vec{H}}{\partial t} \\ \nabla \times \nabla \times \vec{E} &= \nabla (\nabla \cdot \vec{E}) - \Delta \vec{E} = \\ &= -\frac{\mu}{c^2} \frac{\partial \left(\frac{4\pi}{c} \vec{j} + \frac{\epsilon}{c} \frac{\partial \vec{E}}{\partial t} \right)}{\partial t} \\ \Delta \vec{E} - \frac{\epsilon\mu}{c^2} \frac{\partial^2 \vec{E}}{\partial t^2} - \nabla (\nabla \cdot \vec{E}) - \frac{4\pi\mu}{c^2} \frac{\partial \vec{j}}{\partial t} &= 0 \end{aligned}$$

Make component-differentiation (rot rot \rightarrow grad div - laplacian)

Boundary conditions.

Material equations.

- Boundary conditions
- Material equations

$$B_{2n} - B_{1n} = 0$$

$$D_{2n} - D_{1n} = 4\pi\sigma$$

$$E_{2\tau} - E_{1\tau} = 0$$

$$\left(\vec{H}_2 - \vec{H}_1\right) \times \vec{n} = \frac{4\pi \vec{j}}{c}$$

– Isotropic, linear: $\vec{D} = \epsilon \vec{E}$

– Anisotropic: $\vec{D} = \hat{\epsilon} \vec{E}$

– Dispersion: $\vec{D} = \left(1 - \frac{\omega_p^2}{\omega^2}\right) \vec{E}$

– Nonlinear: $\vec{D} = \epsilon \vec{E} + \epsilon_{NL} |\vec{E}|^2 \vec{E}$

Vacuum – Metal boundary - ?

No sources. Plane waves

$$\Delta \vec{E} - \frac{\epsilon\mu}{c^2} \frac{\partial^2 \vec{E}}{\partial t^2} = 0$$

$\vec{A} e^{-i\omega t + ik_z z}$ Observe, that this would satisfy equation

$$-k_z^2 \vec{A} + \frac{\epsilon\mu}{c^2} \vec{A} = 0$$

$k_z^2 = \frac{\epsilon\mu\omega^2}{c^2} = \epsilon\mu k_0^2$ Provided, there is a restriction on k_z and ω

Effective wavelength:

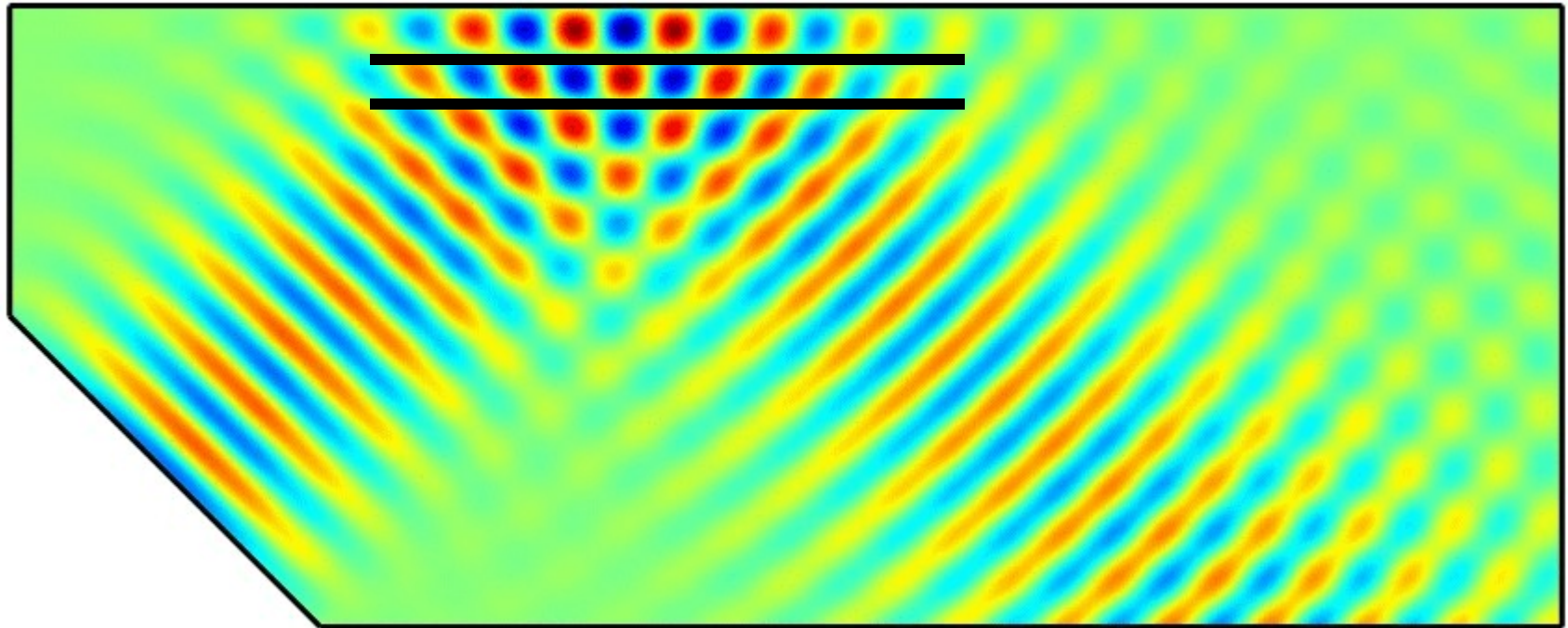
$$\cos(k_z \lambda_{eff}) = 0$$

$$\lambda_{eff} = \frac{2\pi}{k_z}$$

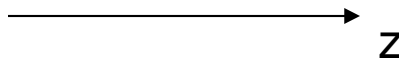
Free – space wavelength

$$\lambda_0 = \frac{2\pi}{k_0} = \frac{c}{f}$$

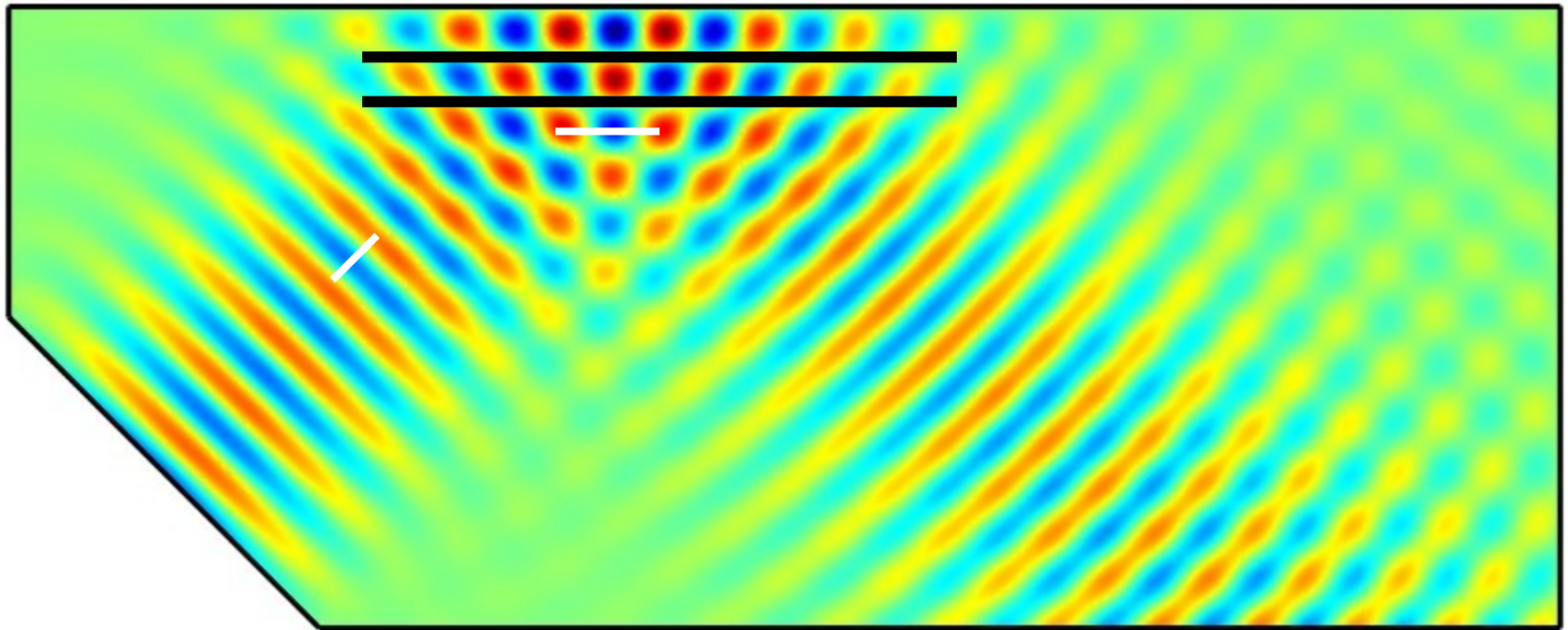
Waveguiding



E_z

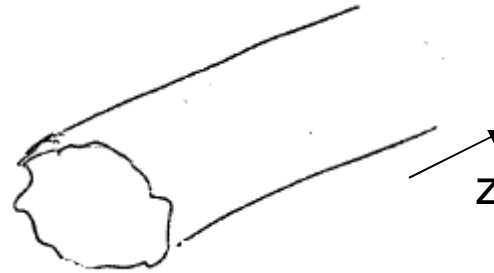


waveguiding



Waveguiding

$$\Delta \vec{E} - \frac{\epsilon\mu}{c^2} \frac{\partial^2 \vec{E}}{\partial t^2} = 0$$



Boundary
condition

Again, searching for
propagating solution

$$\vec{E} = \vec{E}_{\perp}(x, y) e^{-i\omega t + ik_z z}$$

$$E_{z\perp} = 0$$

$$\Delta_{\perp} \vec{E}_{\perp} - k_z^2 \vec{E}_{\perp} + \epsilon\mu k_0^2 \vec{E}_{\perp} = 0$$

For z – component we get

$$\Delta_{\perp} E_{z\perp} - k_z^2 E_{z\perp} + \epsilon\mu k_0^2 E_{z\perp} = 0$$

$$\boxed{\Delta_{\perp} E_{z\perp} = (k_z^2 - \epsilon\mu k_0^2) E_{z\perp}}$$

Has infinitely many solutions,
but there is a way to count
(classify) them

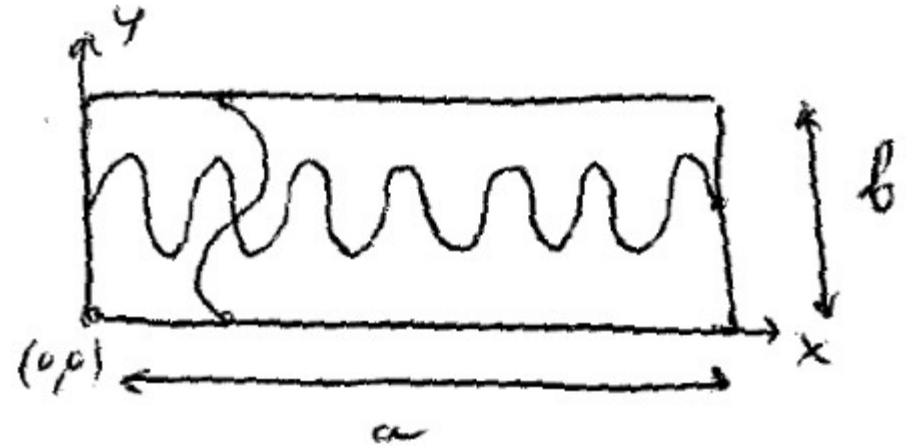
Example: Rectangular waveguide

$$\Delta_{\perp} E_z + \chi^2 E_z = 0$$

$$E_z = X(x) \cdot Y(y)$$

$$\frac{\partial^2 X}{\partial x^2} + \chi_x^2 X = 0$$

$$E_z = E_0 \sin\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right)$$



$$\chi^2 = \left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2$$

Fourier row analogy

Eigenmodes

$$\Delta_{\perp} E_{zi} + \chi_i^2 E_{zi} = \Delta_{\perp} E_{zi} - \lambda_i E_{zi} = 0$$

$$(k_z^2 - \epsilon\mu k_0^2 + \chi_i^2) E_{zi} = 0$$

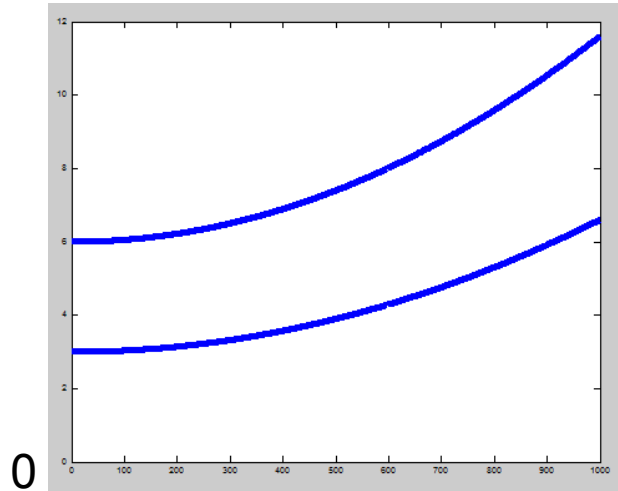
TM $H_z = 0$ vs TE modes

Dispersion $k_z^2 = \epsilon\mu k_0^2 - \chi_i^2$ For i -th mode

What happens if arbitrary field distribution launched from one end into the waveguide at frequency f ?

Dispersion plot

ω



0
0

$$v_{group} = \frac{\partial \omega}{\partial k_z}$$

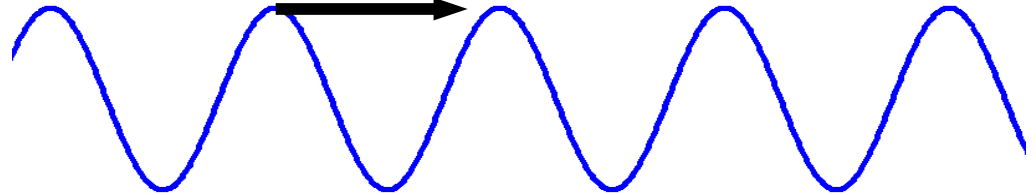
$$k_z^2 = \epsilon \mu k_0^2 - \chi_i^2$$

$$k_0 = \frac{\omega}{c}$$

$$\lambda_{eff} = \frac{2\pi}{k_z}$$

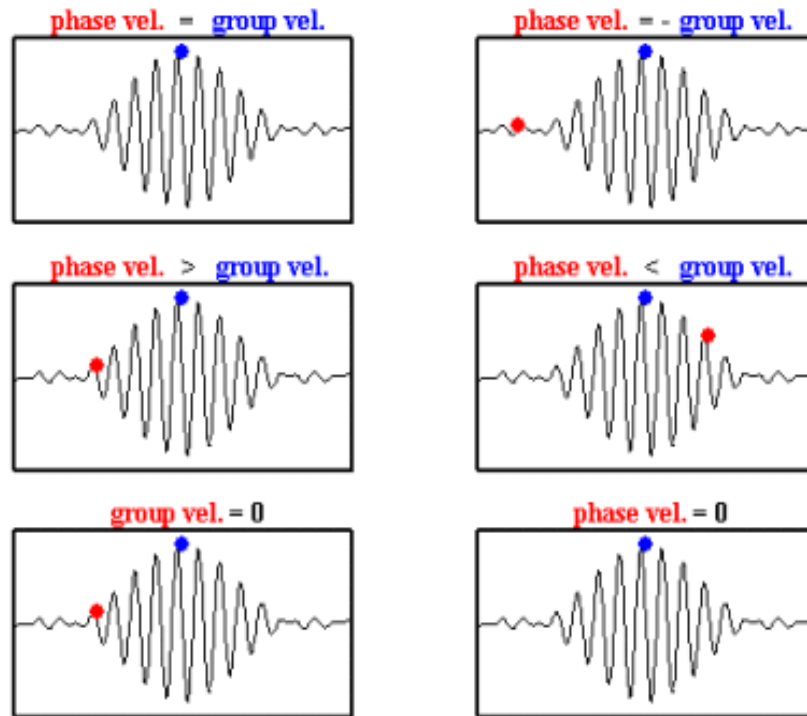
$$T = 2\pi / \omega$$

k_z



$$v_{ph} = \omega / k_z$$

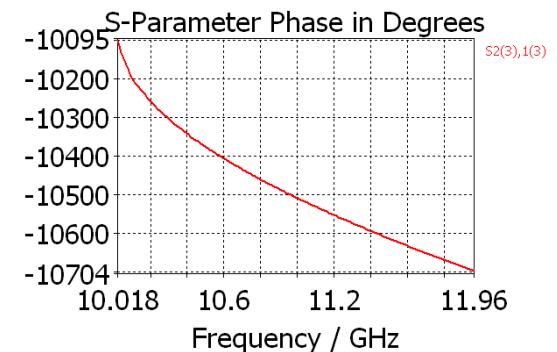
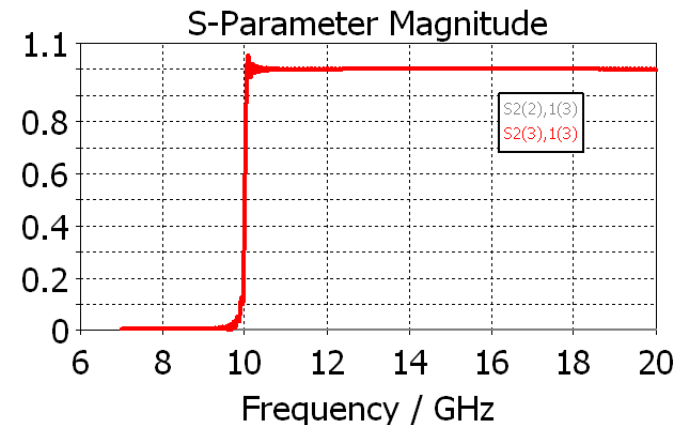
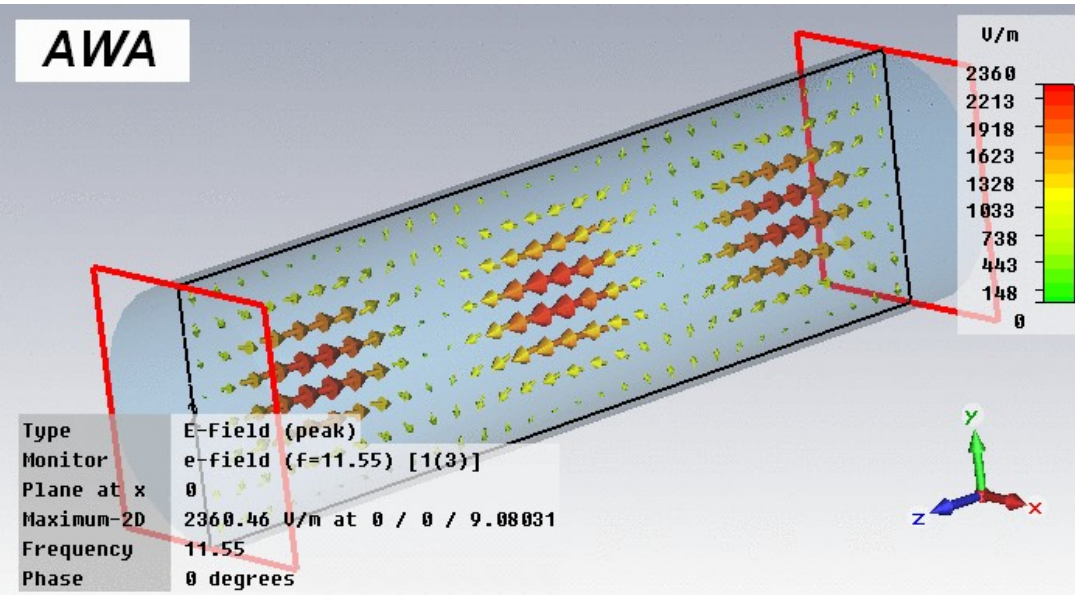
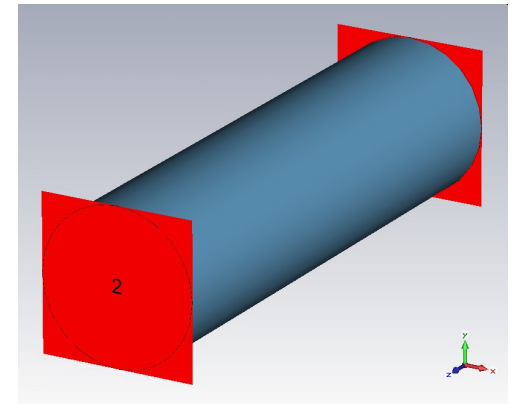
Phase velocity, group velocity



isvr

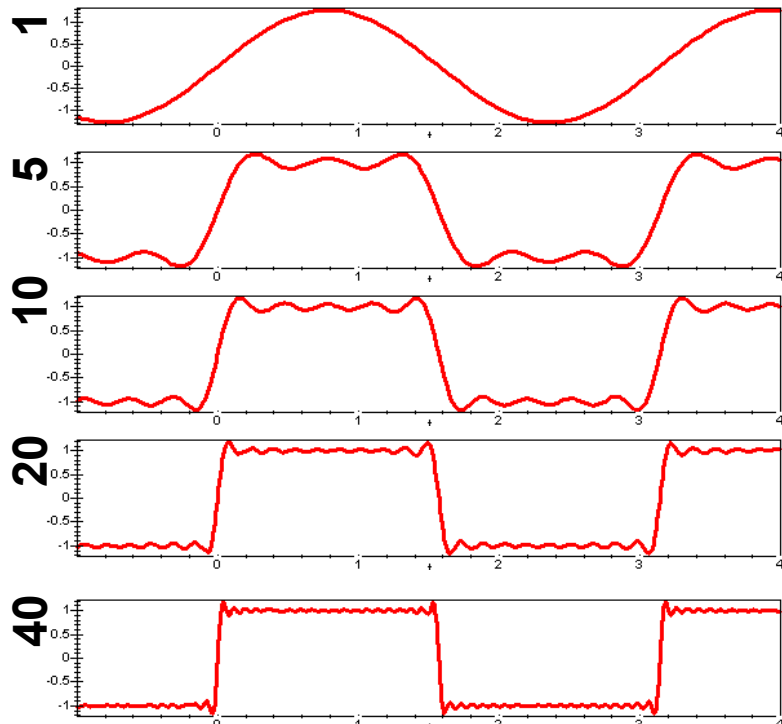
Simulations

- Transmission, S21 / Reflection, S11
- Phase advance $\lambda_{eff} = \frac{2\pi}{k_z}$ vs structure length

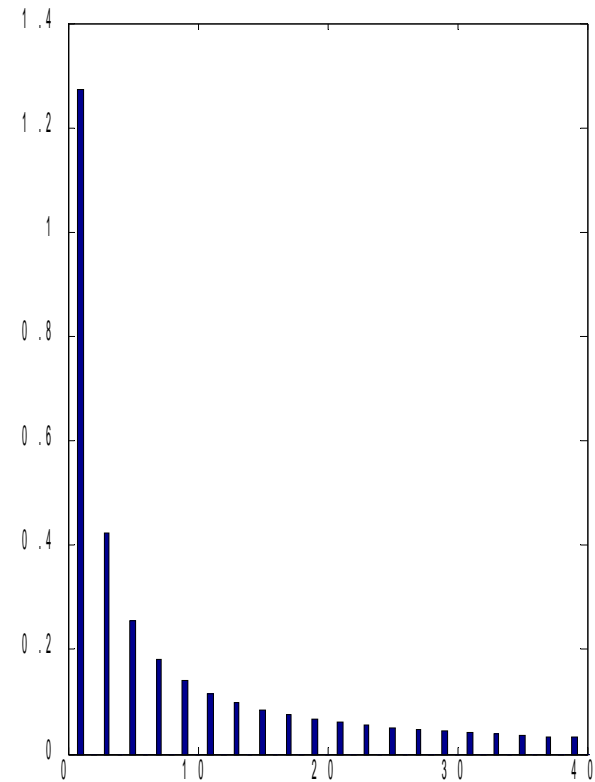


Fourier transform (example: row)

Original periodic signal (bunch train)



spectrum



$$F(t)=1.273*\sin(1*w*t)+0.424*\sin(3*w*t)+0.255*\sin(5*w*t)+0.182*\sin(7*w*t)+0.141*\sin(9*w*t)+0.116*\sin(11*w*t)+0.098*\sin(13*w*t)+0.085*\sin(15*w*t)+0.075*\sin(17*w*t)+0.067*\sin(19*w*t)+0.060*\sin(21*w*t)+0.055*\sin(23*w*t)+0.051*\sin(25*w*t)+0.047*\sin(27*w*t)+0.044*\sin(29*w*t)+0.041*\sin(31*w*t)+0.039*\sin(33*w*t)+0.036*\sin(35*w*t)+0.034*\sin(37*w*t)+0.033*\sin(39*w*t)$$

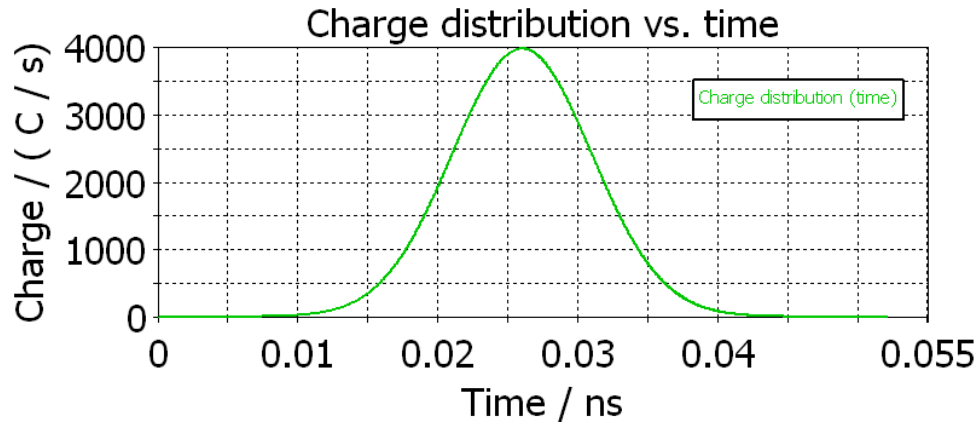
Fourier transform

$$F(\omega) = \int_{-\infty}^{\infty} f(t) e^{i\omega t} dt$$

$$f(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} F(\omega) e^{-i\omega t} d\omega$$

$$j_z = \frac{q}{2\pi} v \cdot \text{Tr}(x, y) \cdot \delta(z - vt)$$

$$j_z = \frac{q}{2\pi} \text{Tr}(x, y) \cdot e^{i\frac{\omega}{v}z}$$



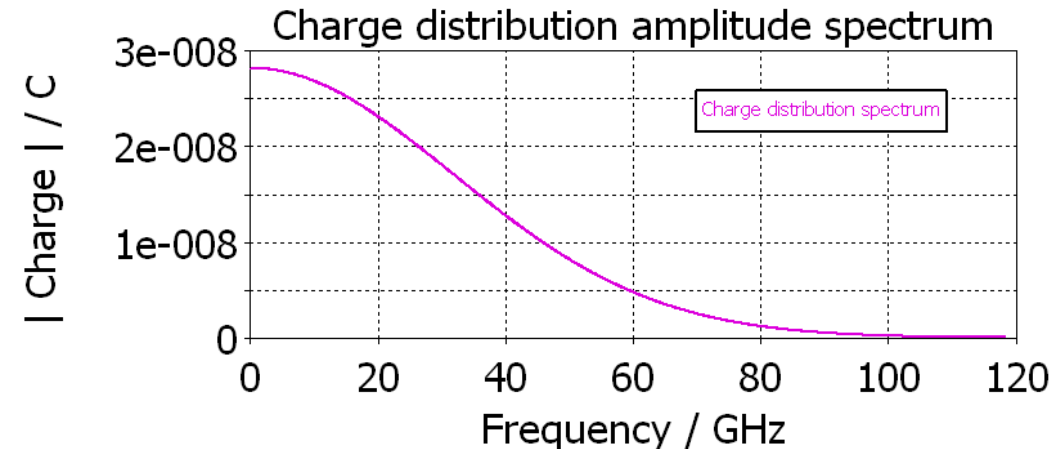
Particle enforces not only frequency, but k_z as well
Phase matching

Delta function / gaussian

Frequency content

Applications in wakefield detection

Applications in simulations



Waveguide + dielectric + beam

$$\Delta E_z - \frac{\epsilon\mu}{c^2} \frac{\partial^2 E_z}{\partial t^2} = \frac{4\pi}{\epsilon} \nabla \rho + \frac{4\pi\mu}{c^2} \frac{\partial j_z}{\partial t}$$

Processes of form:

$$e^{-i\omega t + ik_z(\omega)z}$$

Processes of form:

$$e^{-i\omega t + ik_e(\omega)z}$$

For the particle beam

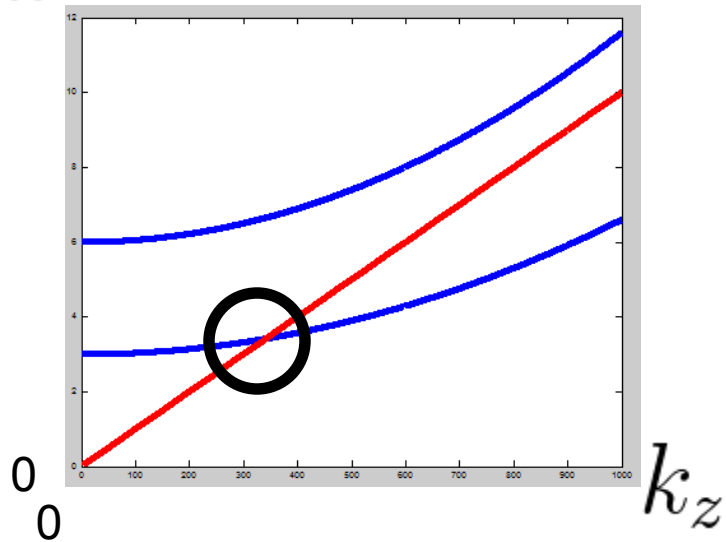
$$\rho, j_z \sim f(z - vt)$$
$$e^{ik_e(z - vt)z}$$

$$k_z^2 = \epsilon\mu k_0^2 - \chi_i^2 \quad \text{AND} \quad k_e = \omega/v$$

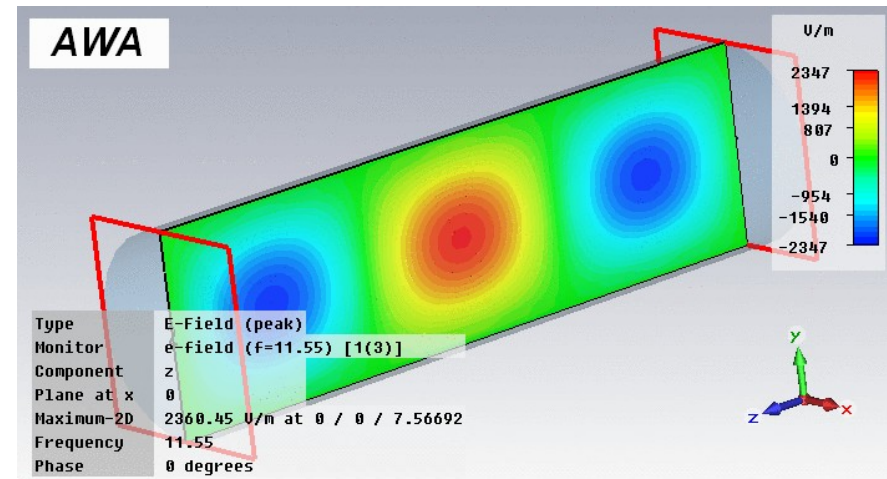
Synchronism

- Phase velocity of the mode should match velocity of a particle

ω



Wakefield



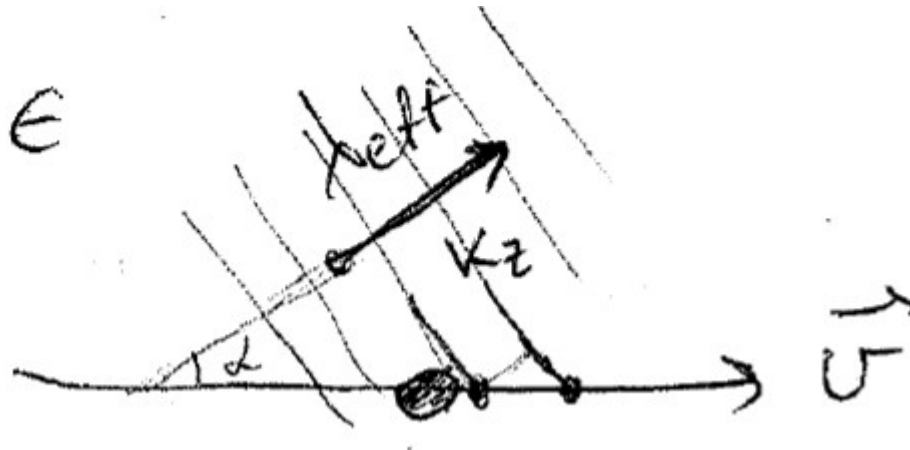
$$k_z^2 = \epsilon \mu k_0^2 - \chi_i^2$$

$$k_z^2 = \frac{\omega^2}{v^2} \quad v = \beta c$$

Vacuum – no interaction

$$\epsilon = \mu = 1$$

Cherenkov radiation



$$v = \beta c$$

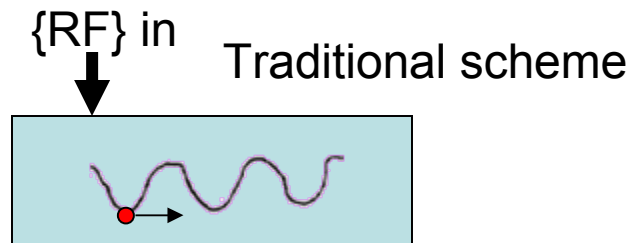
$$\lambda_{trajectory} = \frac{\lambda_{eff}}{\cos\alpha} = \frac{2\pi}{k_z \cos\alpha} = \frac{2\pi c}{\epsilon^{1/2} \cos\alpha \cdot \omega} = vT$$

$$\cos\alpha = \frac{1}{\epsilon^{1/2} \beta}$$

There is a restriction on angle for radiation to occur

Accelerating process

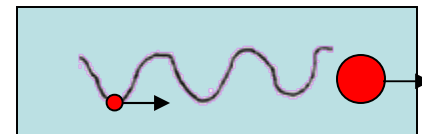
- Particle [electron] energy, velocity ($\approx c$)
- Accelerating structure, that supports mode
- Mode has to have right field pattern
- Mode has to provide synchronization
- Particle interaction with the mode



Standing wave / traveling wave

{RF} source, Coupling

Wakefield acceleration



Drive beam,

timing

Iris-loaded, DLA, PBG, Plasma, Laser-structure ...

What to do with empty waveguide?

empty: $k_{zm}^2 = k_0^2 - \chi_m^2$ $k_0 = \omega/c$

$$k_z^2 = \frac{\omega^2}{v^2} \quad (\text{particle})$$

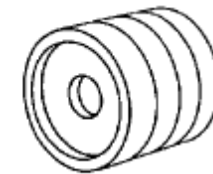
Phase velocity

$$v_{ph} = \frac{\omega}{k_{zm}} = \frac{\omega}{\sqrt{k_0^2 - \chi_m^2}} = \frac{c}{\sqrt{1 - \frac{\chi_m^2 c^2}{\omega^2}}} > c$$

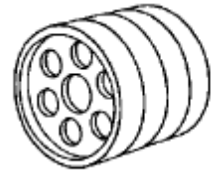
Need to slow mode down

Introduce **any** periodicity

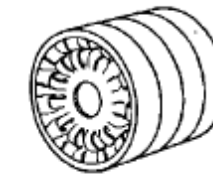
Figure 6-19 Slow-wave structures proposed for linear accelerators.
FORWARD-WAVE STRUCTURES



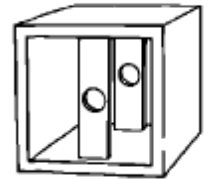
1. DISK-LOADED STRUCTURE



2. VENTILATED STRUCTURE

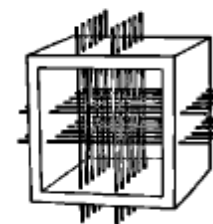


3. CENTIPEDE STRUCTURE



4. RECTANGULAR SLAB

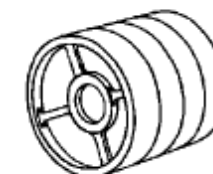
BACKWARD-WAVE STRUCTURES



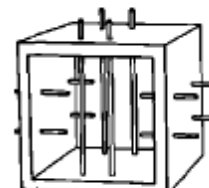
5. 'JUNGLE GYM'



6. SLOTTED DISK STRUCTURE



7. RING & BAR STRUCTURE



8. LOADED EASITRON

The Floquet theorem. Dispersion

- Instead of [empty waveguide]

$$\vec{E} = \vec{E}_{\perp}(x, y)e^{-i\omega t + ik_{z0}z}$$

- We have due to periodicity

$$\vec{E} = \vec{E}_{\perp}(x, y, z)e^{-i\omega t + ik_{z0}z}$$

- Floquet theorem says [kd is a phase advance per period]:

$$E_0(z) = E_0(z + d)e^{\pm ik_0 d}$$

- Fourier row [space harmonics]

$$E(r, z) = \sum_{-\infty}^{\infty} a_n(r)e^{-i\frac{2\pi n}{d}z}$$

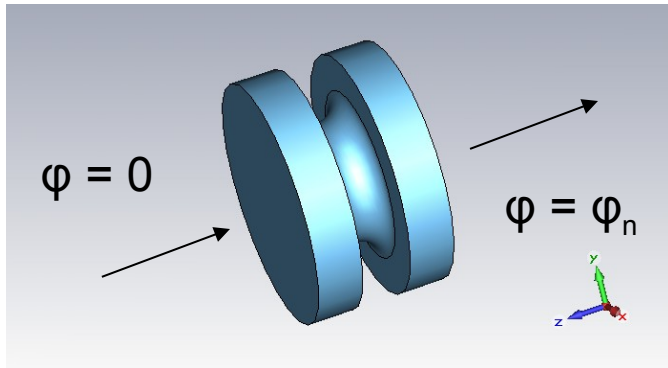
- We end up with effective k_z

$$\vec{E} = \vec{E}_{\perp}(x, y)e^{-i\omega t + ik_z z + i\frac{2\pi n}{d}z}$$

simulations

- Corrugated structure:
- Periodic cells:
 - Phase advance and dispersion
 - Space harmonics
- Eigenmodes.
- Geometry optimization
- All set to calculate accelerating parameters

Dispersion

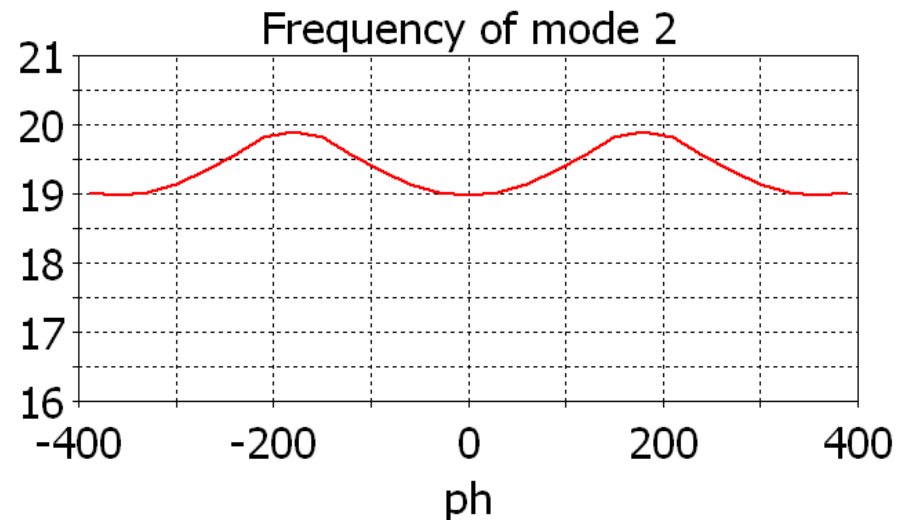
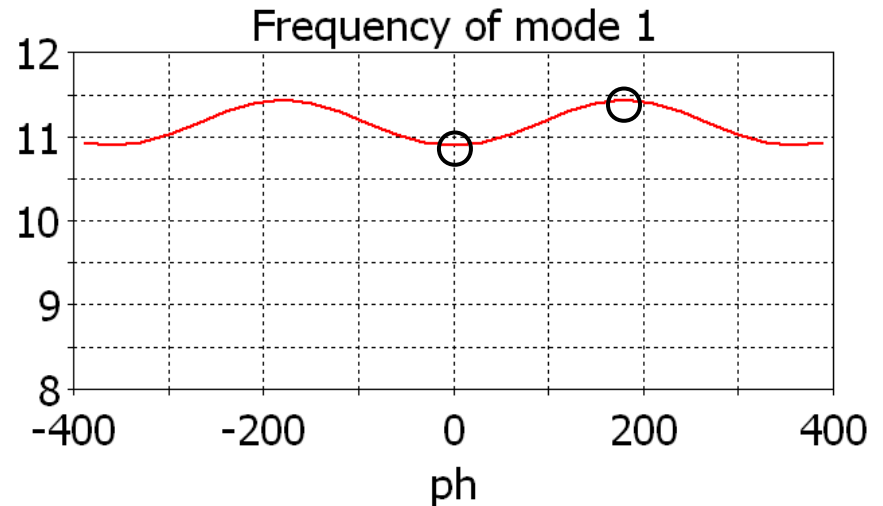


$k_z \cdot d$ – phase advance

Synchronization with particle is guaranteed!

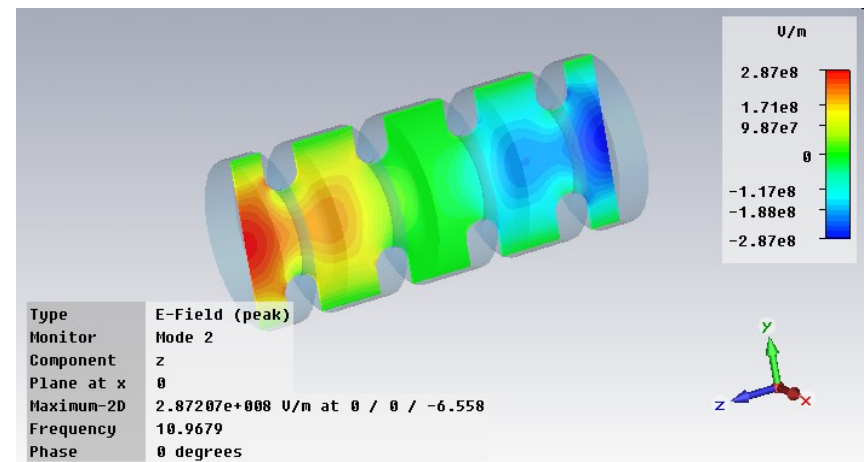
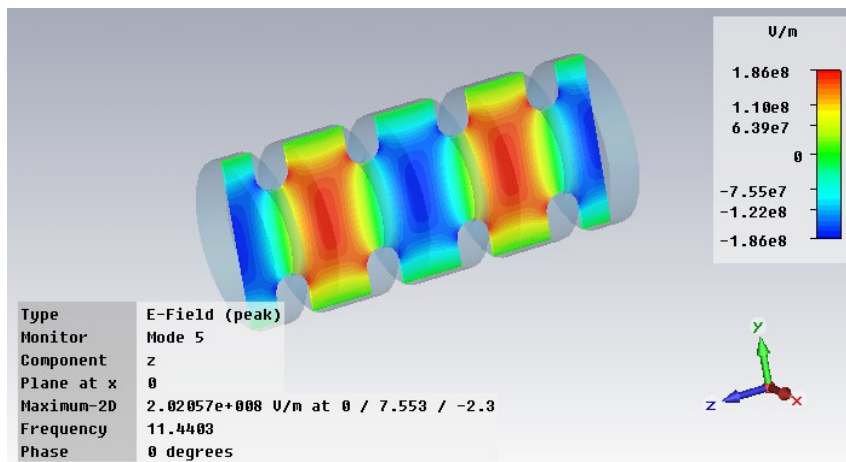
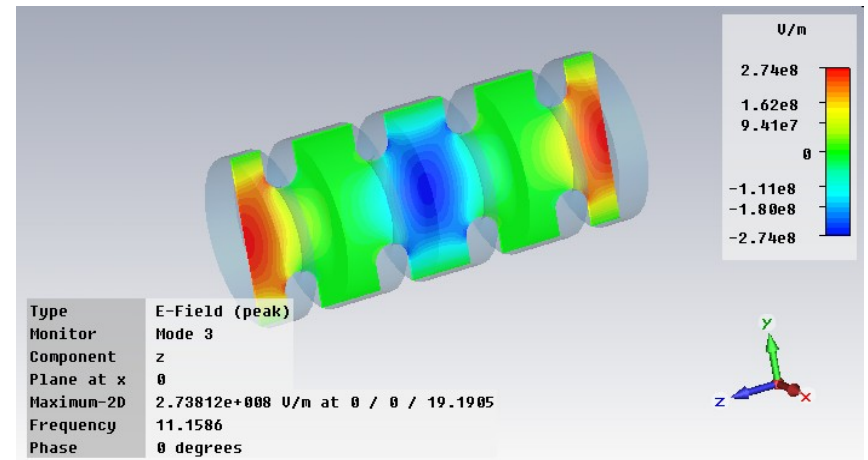
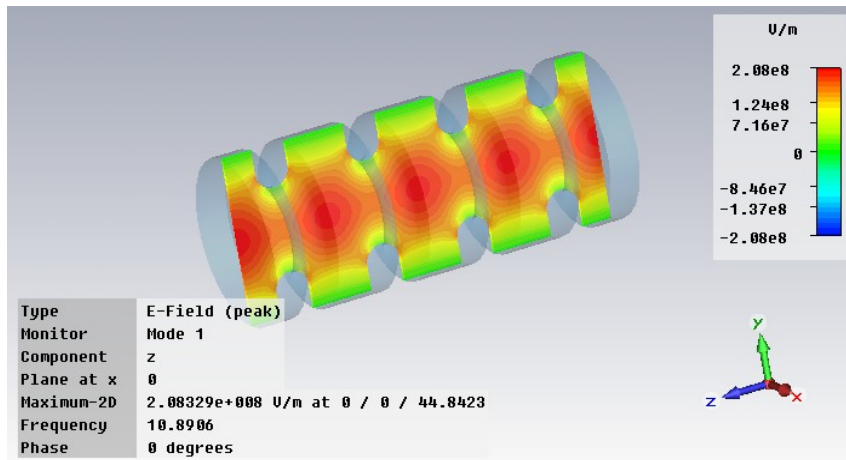
There are forbidden bands. Why?!

Theme alert 😊

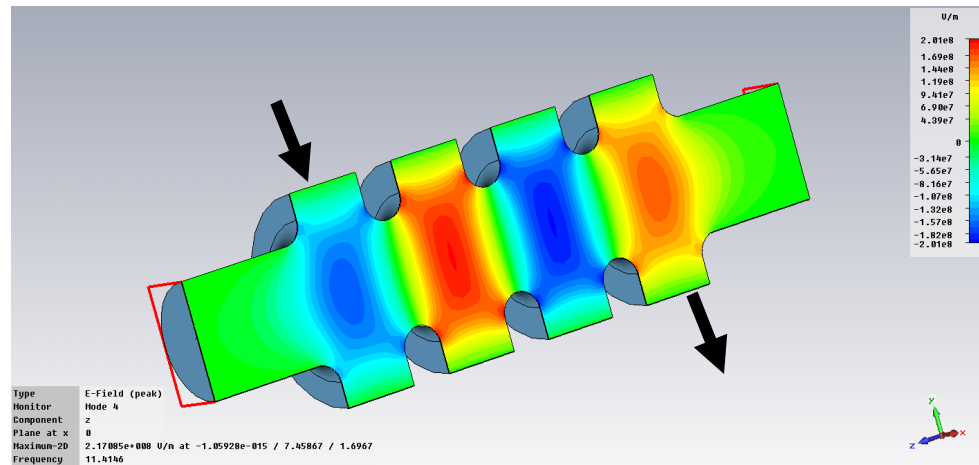


- Travelling wave accelerator vs Standing wave accelerator

Phase advance per cell

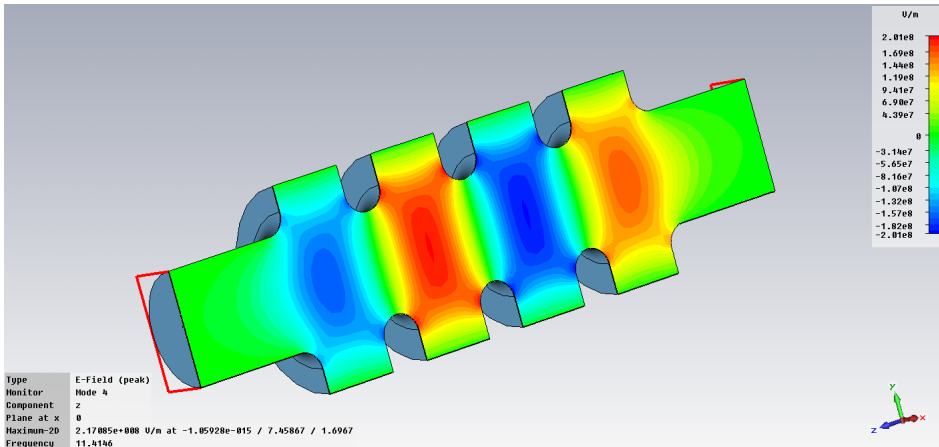


Iris – loaded waveguide



- Corrugation – form of periodicity in this case
- Period – cell length
- Alternative interpretation: coupled pill – box cavities (set of coupled oscillators)
- Travelling wave accelerator vs Standing wave accelerator

Transit effect simulation



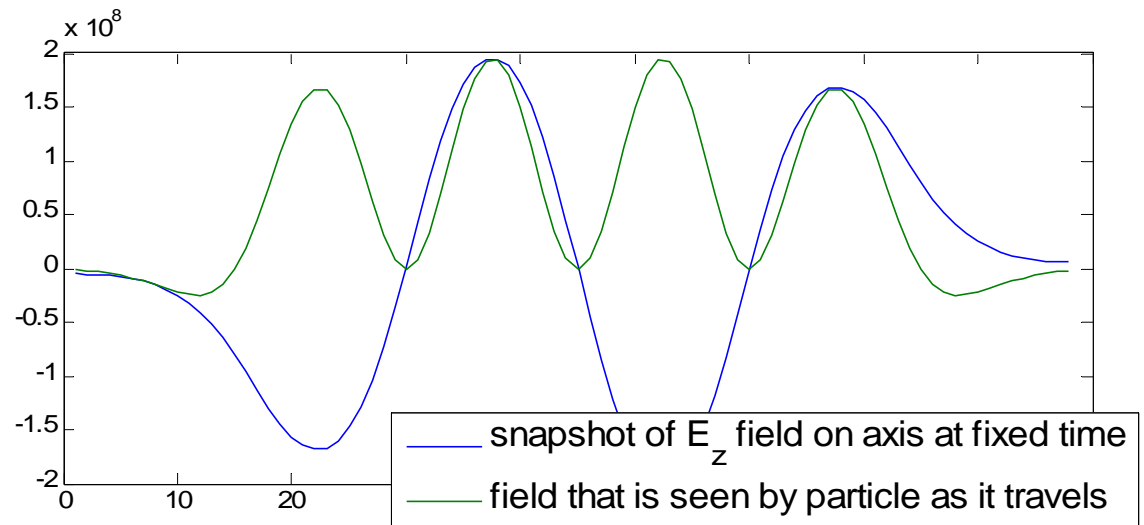
$$\Delta W = q \int_{-L/2}^{L/2} E(0, z) \cos(\omega t(z) + \phi) dz$$

$$\omega t = \omega z / v = 2\pi z / \beta \lambda$$

$$T = \frac{\int_{-L/2}^{L/2} E(0, z) \cos(2\pi z / \beta \lambda) dz}{\int_{-L/2}^{L/2} E(0, z) dz}$$

Panofsky equation:
energy gain

$$\Delta W = q E_0 T \cos(\phi L)$$



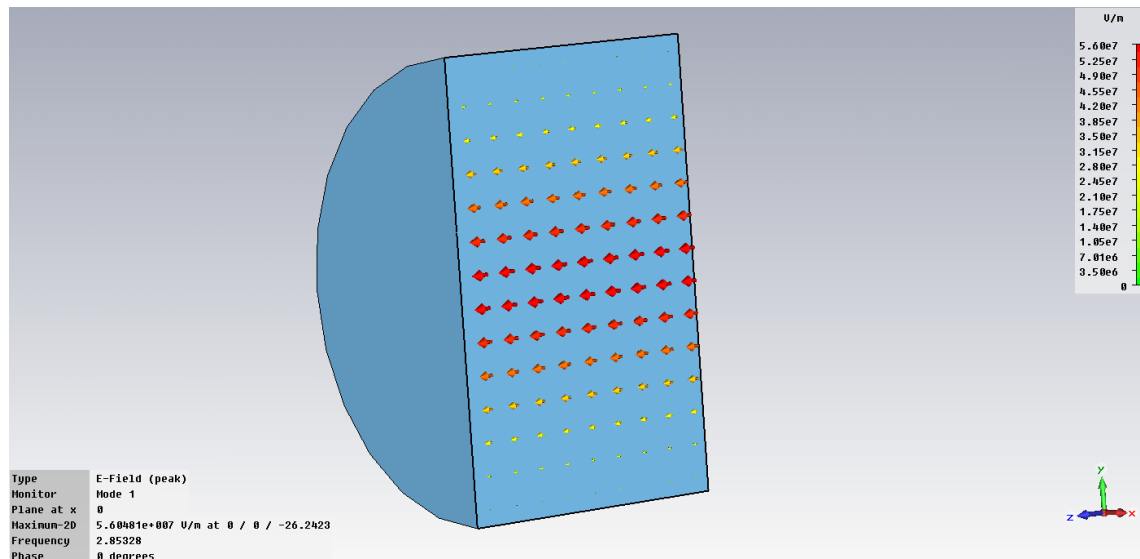
Transient effect simulation

- SW_3_cells_parameters_accelerator.cst
- D=8.7474 mm cell [optimize] for 11.424 GHz for $2\pi/3$
- Template based postprocessing
 - Evaluate field along arbitrary coordinates
 - 1D result from 1D result, rescale
- Export to matlab
- `plot(ez(:,1),[-(ez(:,2)) ez(:,2).*scale(:,2)])`
- `T=sum(ez(:,2).*scale(:,2))/sum(abs(ez(:,2)))`

Analogous to:

$$T = \frac{\int_{-L/2}^{L/2} E(0, z) \cos(2\pi z / \beta \lambda) dz}{\int_{-L/2}^{L/2} E(0, z) dz}$$

Accelerating parameters of a pillbox SW cavity



TM₀₁₀ mode @ 2.856 GHz

$\lambda_0 = 104.97 \text{ mm}$

$a = 40.1789 \text{ mm}$

$d = 52.4847 \text{ mm}$

$E_0 = 56 \text{ MV/m}$

Cavity parameters

*For TW define per unit length

$$U = \frac{\epsilon}{2} \int_V \vec{E}^2 dV$$

Stored energy = 1 Joule

$$P = \frac{R_s}{2} \int_S H^2 dS$$

Power dissipation = 968 kWatt

$$Q = \frac{\omega U}{P}$$

Quality factor = 18500

$$T = \frac{\int_{-L/2}^{L/2} E(0, z) \cos(2\pi z / \beta \lambda) dz}{\int_{-L/2}^{L/2} E(0, z) dz}$$

Transit factor = .64

$$T \cdot E_0$$

Effective gradient = 35.7 MV/m

$$T \cdot E_0 \cdot d$$

Panofsky voltage / energy gain = 1.87 MeV

$$R_{sh} = (T \cdot E_0 \cdot d)^2 / P$$

per structure

Effective shunt impedance = 3.6 MOhm

$$r_{sh} = (T \cdot E_0 \cdot d)^2 / P / d$$

per unit length

Effective shunt impedance = 69 MOhm/m

$$R_{sh} / Q$$

per structure

Effective R over Q = 196 Ohms

$$R_{sh} / Q / d$$

per unit length

Effective R over Q = 3.7 kOhm/m

Accelerating parameters

- Shunt impedance measures efficiency of acceleration for a given dissipated power
- r / Q shows how much accelerating field one has for a given stored energy; depends on geometry only as loss excluded
-

Computer lab / homework

- Simulate X-Band iris loaded structure
- Optimize geometry to match [$\pi/3$, $2\pi/3$, $\pi/4$ mode] to 11.424 GHz
- Calculate
 - Transit factor
 - Q, R/Q, R
 - ...